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## Casimir effect across a layered medium

Marin-Slobodan Tomaš

*Rudjer Bošković Institute, P. O. B. 180, 10002 Zagreb, Croatia*  
*tomas@thphys.irb.hr*

Using nonstandard recursion relations for Fresnel coefficients involving successive stacks of layers, we extend the Lifshitz formula to configurations with an inhomogeneous,  $n$ -layered, medium separating two planar objects. The force on each object is the sum of a Lifshitz like force and a force arising from the inhomogeneity of the medium. The theory correctly reproduces very recently obtained results for the Casimir force/energy in some simple systems of this kind. As a by product, we obtain a formula for the force on an (unspecified) stack of layers between two planar objects which generalizes our previous result for the force on a slab in a planar cavity.

*Keywords:* Casimir force; Fresnel coefficients; nonstandard recursion.

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### 1. Introduction

Very recently, several papers appeared dealing with the theory of the Casimir effect in systems consisting of two perfectly reflecting plates separated by a layered medium<sup>1,2,3</sup>. Among the other results, these works provided formulas for the Casimir force and/or energy for a few simple systems of this sort (with up to five layers media<sup>1</sup> between the plates). Using the theory of the Casimir effect in multilayers<sup>4</sup> and nonstandard recursion relations for Fresnel coefficients<sup>4,5,6,7</sup>, in this Note we derive formulas for the Casimir force and energy for systems with arbitrary plates separated by arbitrary inhomogeneous, generally  $n$ -layered, media.

### 2. Casimir effect across a layered medium

Consider the system consisting of two planar objects (plates) separated by a layered medium, as depicted in Fig. 1. According to the theory of the Casimir effect in multilayers<sup>4</sup>, the Casimir forces on the left ( $L$ ) and the right ( $R$ ) plate are given by

$$F_L \equiv F_{1-} = T_{zz}^{(1)} \quad \text{and} \quad F_R \equiv F_{n+} = -T_{zz}^{(n)}, \quad (1)$$

respectively, where (unless necessary, we omit the polarization index  $q = p, s$  when writing Fresnel coefficients)

$$T_{zz}^{(j)} = \frac{\hbar}{2\pi^2} \int_0^\infty d\xi \int_0^\infty dk k \kappa_j \sum_q \frac{r_{j-} r_{j+} e^{-2\kappa_j d_j}}{1 - r_{j-} r_{j+} e^{-2\kappa_j d_j}} \quad (2)$$

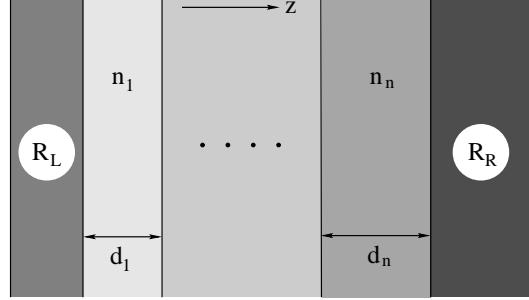


Fig. 1. Two plates separated by a layered medium shown schematically. Plates are described by their reflection coefficients  $R_L$  and  $R_R$  and the medium layers by their (complex) refraction indexes  $n_a(\omega) = \sqrt{\varepsilon_a(\omega)\mu_a(\omega)}$ ,  $a = 1 \dots n$ .

is the relevant component of the vacuum-field (Minkowski) stress tensor in the layer  $j$ . Here  $\kappa_j = \sqrt{n_j^2(i\xi)\xi^2/c^2 + k^2}$  is the perpendicular wave vector at the imaginary frequency ( $\omega = i\xi$ ) in the layer,  $k = \sqrt{k_x^2 + k_y^2}$  is the magnitude of the wave vector parallel to the system surfaces and  $r_{j\pm}(i\xi, k)$  are the reflection coefficients of the right and left stack of layers bounding the layer  $j$ . These reflection coefficients obey generalized recursion relations<sup>4,5,6,7</sup>

$$r_{j\pm} = r_{j/l} + \frac{t_{j/l} r_{l\pm} e^{-2\kappa_l d_l}}{1 - r_{l/j} r_{l\pm} e^{-2\kappa_l d_l}}, \quad t_{j\pm} = \frac{t_{j/l} t_{l\pm} e^{-\kappa_l d_l}}{1 - r_{l/j} r_{l\pm} e^{-2\kappa_l d_l}}, \quad (3)$$

where  $l$  denotes an intermediate layer and where the symbol  $a/b \equiv a \dots b$  is used to denote the stack of layers between layers  $a$  and  $b$ . As seen, these recurrence relations look the same as the standard ones<sup>8,9</sup> (to which they reduce in case that layers  $j$  and  $l$  are neighbor layers), however, this time they generally involve Fresnel coefficients  $r_{j/l}$ ,  $r_{l/j}$ ,  $t_{j/l}$  and  $t_{l/j}$  of the *stack* between the layers  $j$  and  $l$ .

Using the above recursion relations, reflection coefficients  $r_{1+}$  and  $r_{n-}$  can be expressed as

$$r_{1+} = \frac{r_{1/n} + a_{1/n} R_R e^{-2\kappa_n d_n}}{1 - r_{n/1} R_R e^{-2\kappa_n d_n}}, \quad r_{n-} = \frac{r_{n/1} + a_{n/1} R_L e^{-2\kappa_1 d_1}}{1 - r_{1/n} R_L e^{-2\kappa_1 d_1}}, \quad (4)$$

where we have introduced the quantity

$$a_{1/n} = t_{1/n} t_{n/1} - r_{1/n} r_{n/1} = a_{n/1} \quad (5)$$

and identified  $r_{n+}$  and  $r_{1-}$  as the reflection coefficients  $R_R$  and  $R_L$ , respectively, of the plates. Therefore, from (1) and (2) we obtain for the forces on the plates

$$F_L = \frac{\hbar}{2\pi^2} \int_0^\infty d\xi \int_0^\infty dk \kappa_1 \sum_q \frac{1}{N_n} (r_{1/n} + a_{1/n} R_R e^{-2\kappa_n d_n}) R_L e^{-2\kappa_1 d_1}, \quad (6a)$$

$$F_R = \frac{-\hbar}{2\pi^2} \int_0^\infty d\xi \int_0^\infty dk \kappa_n \sum_q \frac{1}{N_n} (r_{n/1} + a_{n/1} R_L e^{-2\kappa_1 d_1}) R_R e^{-2\kappa_n d_n}, \quad (6b)$$

where

$$N_n = 1 - (r_{1/n} R_L e^{-2\kappa_1 d_1} + r_{n/1} R_R e^{-2\kappa_n d_n}) - a_{1/n} R_L R_R e^{-2\kappa_1 d_1 - 2\kappa_n d_n}. \quad (7)$$

As seen, since  $r_{1/n} \neq r_{n/1}$  unless the medium is not symmetric across the gap, these forces are not generally equal in magnitude and each of them consists of a Lifshitz-like force (given by the second terms in (6)) and a force due to the inhomogeneity of the medium. We also note that owing to the medium inhomogeneity there is a force<sup>4</sup>  $F_S = T_{zz}^{(n)} - T_{zz}^{(1)} = -F_R - F_L$  on the central stack of the medium given explicitly by

$$F_S = \frac{\hbar}{2\pi^2} \int_0^\infty d\xi \int_0^\infty dk k \sum_q \frac{1}{N_n} (\kappa_n r_{n/1} R_R e^{-2\kappa_n d_n} - \kappa_1 r_{1/n} R_L e^{-2\kappa_1 d_1}) + (\kappa_n - \kappa_1) \frac{a_{1/n}}{N_n} R_L R_R e^{-2\kappa_1 d_1 - 2\kappa_n d_n}. \quad (8)$$

When  $n_1 = n_n$ , this generalizes previously obtained result for the force on a slab in a planar cavity<sup>4,7,10</sup> to configurations with the slab replaced by an unspecified multilayered stack.

Having determined forces on the plates, we can calculate the Casimir energy of the system from<sup>4</sup>  $F_L = \partial E / \partial d_1$  or  $F_R = -\partial E / \partial d_n$ . We obtain

$$E = \frac{\hbar}{(2\pi)^2} \int_0^\infty d\xi \int_0^\infty dk k \sum_q \ln N_n. \quad (9)$$

In the following, we illustrate this formula by discussing its implications for several simple systems and comparing them with the results obtained in Refs. 1-3.

### 3. Discussion

It is easy to see that (7) and (9) give correctly the Casimir energy in case of a homogeneous medium between the plates. Indeed, assuming that all  $n$  medium layers are made of the same matter ( $n_a = n$ ,  $\kappa_a = \kappa$ ), we have  $r_{1/n} = r_{n/1} = 0$  and  $t_{1/n} = t_{n/1} = \exp[-\kappa(d - d_1 - d_n)]$  so that  $a_{1/n} = \exp[-2\kappa(d - d_1 - d_n)]$  and

$$N_n = 1 - R_L R_R e^{-2\kappa d}, \quad (10)$$

where  $d$  is the distance between the plates. This leads to the standard Lifshitz-type formula<sup>11</sup> for the Casimir energy. For perfectly reflecting plates<sup>2,3</sup>, we must let here  $R_L R_R = 1$ .

In the  $n = 2$  case (two media between the plates), we have  $r_{1/2} = r_{12} = -r_{21} = -r_{2/1}$  and  $t_{1/2} = t_{12} = (\mu_2 \kappa_1 / \mu_1 \kappa_2) t_{21} = (\mu_2 \kappa_1 / \mu_1 \kappa_2) t_{2/1}$ , where  $r_{12}$  and  $t_{12}$  are the *single-interface* Fresnel coefficients<sup>4,5</sup>

$$r_{12} = \frac{\kappa_1 - \gamma_{12} \kappa_2}{\kappa_1 + \gamma_{12} \kappa_2} = -r_{21}, \quad t_{12} = \sqrt{\frac{\gamma_{12}}{\gamma_{12}^s}} (1 + r_{12}) = \frac{\mu_2 \kappa_1}{\mu_1 \kappa_2} t_{21}, \quad (11)$$

with  $\gamma_{12}^p = \varepsilon_1 / \varepsilon_2$  and  $\gamma_{12}^s = \mu_1 / \mu_2$ . Noting that  $a_{1/2} = 1$ , we have

$$N_2 = 1 - r_{12} (R_L e^{-2\kappa_1 d_1} - R_R e^{-2\kappa_2 d_2}) - R_L R_R e^{-2(\kappa_1 d_1 + \kappa_2 d_2)}, \quad (12)$$

which, in conjunction with (9), gives the Casimir energy for the present system. This result coincides with the corresponding result obtained in Ref. 2 providing that we let for perfectly reflecting plates  $R_{L(R)}^q = -1$ . We note, however, that perfect reflectors are standardly simulated by media with infinitely large permittivities (conductivities) in which case (11) implies ( $\varepsilon_2 \rightarrow \infty$ ) that  $R_{L(R)}^s = -1$  but  $R_{L(R)}^p = 1$ . Therefore, with this convention, our result disagrees with that of Ref. 2 regarding the  $p$  contribution to the Casimir force/energy.

Using recursion relations (3), E for more complex ( $n \geq 3$ ) systems can be written in terms of lower-layered stacks and, owing to the number of the medium layers, this can be done in a number of ways. Clearly, to obtain the effective Casimir energy, we can drop from these results the terms not involving  $d_1$  or  $d_n$ . Thus, for example, from (3) we have<sup>7</sup>

$$r_{1/n} = \frac{r_{1/l} + a_{1/l} r_{l/n} e^{-2\kappa_l d_l}}{D_l}, \quad r_{n/1} = \frac{r_{n/l} + a_{n/l} r_{l/1} e^{-2\kappa_l d_l}}{D_l}, \quad (13a)$$

$$a_{1/n} = \frac{a_{1/l} a_{n/l} e^{-2\kappa_l d_l} - r_{1/l} r_{n/l}}{D_l}, \quad D_l = 1 - r_{l/1} r_{l/n} e^{-2\kappa_l d_l}. \quad (13b)$$

Using this in (7) and rearranging, we find

$$N_n = \frac{N_n^{(l)}}{D_l}, \quad (14)$$

where

$$N_n^{(l)} = (1 - r_{1/l} R_L e^{-2\kappa_1 d_1})(1 - r_{n/l} R_R e^{-2\kappa_n d_n}) - e^{-2\kappa_l d_l} (a_{1/l} R_L e^{-2\kappa_1 d_1} + r_{l/1})(a_{n/l} R_R e^{-2\kappa_n d_n} + r_{l/n}). \quad (15)$$

Finally, inserting this  $N_n$  in (9) and dropping the (ineffective) term involving  $D_l$ , we find for the effective Casimir energy  $E_l$  of the system (with respect to the layer  $l$ )

$$E_l = \frac{\hbar}{(2\pi)^2} \int_0^\infty d\xi \int_0^\infty dk \sum_q \ln N_n^{(l)}. \quad (16)$$

This generalizes the ( $T = 0$ ) result for the Casimir interaction energy between two slabs obtained in Ref 1 using a realistic Casimir piston approach and a five layer model for the medium to arbitrary multilayered slabs and plates. Note that, when removing the plates by letting  $d_{1(n)} \rightarrow \infty$ , we have  $N_n^{(l)} \rightarrow D_l$  and (15) and (16) give the Casimir interaction energy of the two stacks of layers separated by a layer of medium  $l$ , as derived in Ref. 4.

We illustrate the above result by considering the  $n=3$  system. In this case, there is only one intermediate layer and the effective Casimir energy (16) is entirely expressed in terms of the single-interface reflection coefficients  $r_{12} = -r_{21}$  and  $r_{32} = -r_{23}$ . From (15), we have ( $a_{1/2} = a_{3/2} = 1$ )

$$N_3^{(2)} = (1 - r_{12} R_L e^{-2\kappa_1 d_1})(1 - r_{32} R_R e^{-2\kappa_3 d_3}) - e^{-2\kappa_2 d_2} (R_L e^{-2\kappa_1 d_1} - r_{12})(R_R e^{-2\kappa_3 d_3} - r_{32}). \quad (17)$$

As mentioned, for perfectly reflecting plates we must let here  $R_{L(R)}^q = \delta_{qp} - \delta_{qs}$ . This result then coincides with the corresponding result derived in Ref. 1 whereas the results obtained in Refs. 2 and 3 correspond to plates with  $R_{L(R)}^q = -1$  and  $R_{L(R)}^q = 1$ , respectively.

#### 4. Summary

Effectively, in this work we have extended the Lifshitz formula to configurations with an inhomogeneous, n-layered, medium separating two planar objects. The force on each object is the sum of a Lifshitz-like force and a force arising from the inhomogeneity of the medium. Owing to this inhomogeneity, there is also a force acting on the medium. When the first and the last medium layer are made of the same matter, this result generalizes previously obtained one for the force on a slab in a planar cavity to arbitrary multilayered slabs.

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